

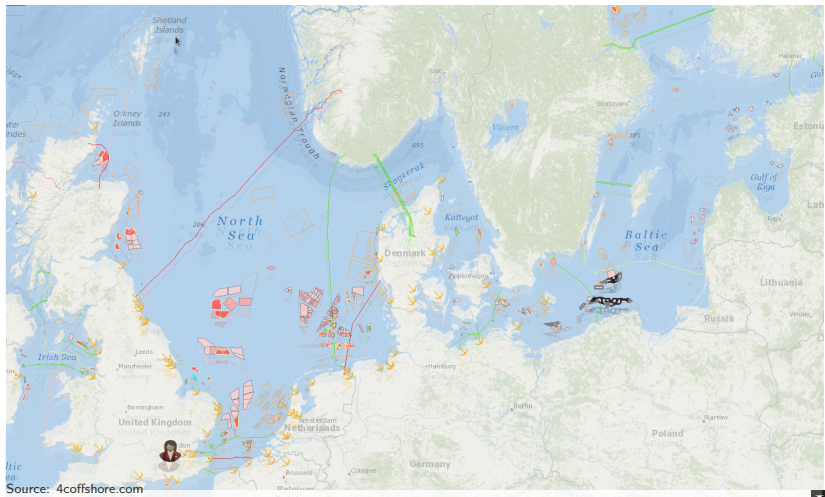
Predicting Offshore Wind Farm Cluster Performance Using RaNS-based Actuator Disc Wind Turbine Model

Vitor M. M. G. da Costa Gomes
José M. L. M. da Palma

CEsA – *Centre for Wind Energy and Atmospheric Flows*
FEUP – *Faculty of Engineering of the University of Porto*
Portugal

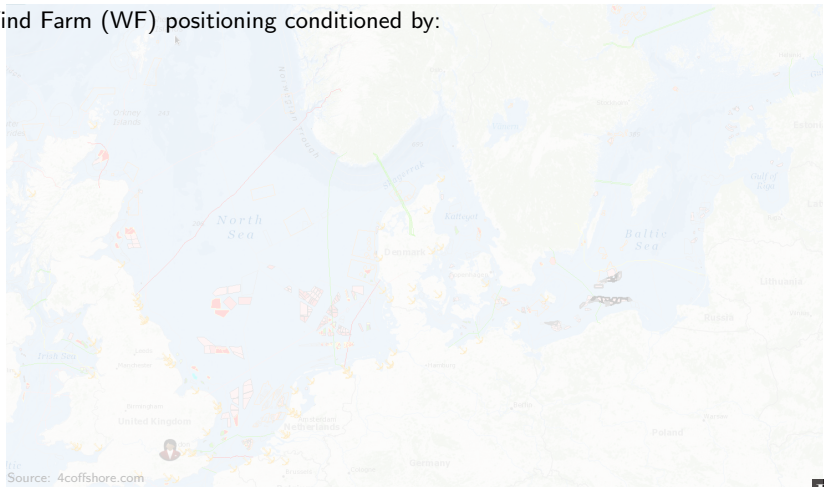
29th April 2015

EU Offshore Wind Energy Challenges



EU Offshore Wind Energy Challenges

Wind Farm (WF) positioning conditioned by:



EU Offshore Wind Energy Challenges

Wind Farm (WF) positioning conditioned by:

- High wind resource availability;
- Low water depths;
- On-shore grid connection availability.

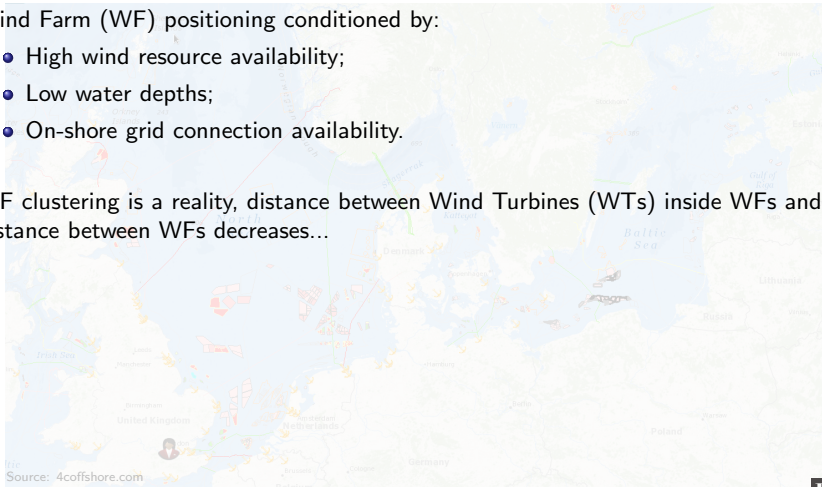


EU Offshore Wind Energy Challenges

Wind Farm (WF) positioning conditioned by:

- High wind resource availability;
- Low water depths;
- On-shore grid connection availability.

WF clustering is a reality, distance between Wind Turbines (WTs) inside WFs and distance between WFs decreases...



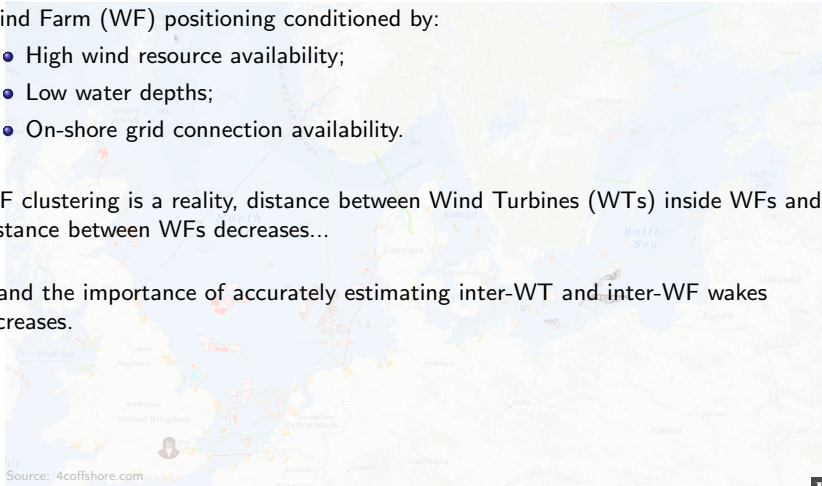
EU Offshore Wind Energy Challenges

Wind Farm (WF) positioning conditioned by:

- High wind resource availability;
- Low water depths;
- On-shore grid connection availability.

WF clustering is a reality, distance between Wind Turbines (WTs) inside WFs and distance between WFs decreases...

...and the importance of accurately estimating inter-WT and inter-WF wakes increases.



EU Offshore Wind Energy Challenges

Wind Farm (WF) positioning conditioned by:

- High wind resource availability;
- Low water depths;
- On-shore grid connection availability.



WF clustering is a reality, distance between Wind Turbines (WTs) inside WFs and distance between WFs decreases...

...and the importance of accurately estimating inter-WT and inter-WF wakes increases.

Wake model developed over an in-house developed CFD tool (VENTOS[®]), under the EU project EERA-DTOC (3).

Source: 4coffshore.com

VENTOS[®]/2 software

Non-linear CFD code geared towards solving wind flow problems over complex terrain (1; 4):



VENTOS[®]/2 software

Non-linear CFD code geared towards solving wind flow problems over complex terrain (1; 4):

- Elliptic Finite-volume Reynold averaged Navier-Stokes solver for non-stratified flows;



VENTOS[®]/2 software

Non-linear CFD code geared towards solving wind flow problems over complex terrain (1; 4):

- Elliptic Finite-volume Reynold averaged Navier-Stokes solver for non-stratified flows;
- Two-equation $k-\varepsilon$ turbulence model;



VENTOS[®]/2 software

Non-linear CFD code geared towards solving wind flow problems over complex terrain (1; 4):

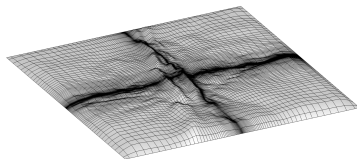
- Elliptic Finite-volume Reynold averaged Navier-Stokes solver for non-stratified flows;
- Two-equation $k-\varepsilon$ turbulence model;
- Solution as steady-state or time-dependent problem;



VENTOS[®]/2 software

Non-linear CFD code geared towards solving wind flow problems over complex terrain (1; 4):

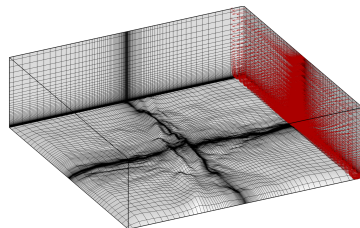
- Elliptic Finite-volume Reynold averaged Navier-Stokes solver for non-stratified flows;
- Two-equation $k-\varepsilon$ turbulence model;
- Solution as steady-state or time-dependent problem;
- Structured, horizontally orthogonal, terrain-following mesh to capture topography;



VENTOS[®]/2 software

Non-linear CFD code geared towards solving wind flow problems over complex terrain (1; 4):

- Elliptic Finite-volume Reynold averaged Navier-Stokes solver for non-stratified flows;
- Two-equation $k-\varepsilon$ turbulence model;
- Solution as steady-state or time-dependent problem;
- Structured, horizontally orthogonal, terrain-following mesh to capture topography;
- Channel-like domain, with static boundary conditions.



WT wake modelling in VENTOS[®]/2...

Wind Turbine (WT) rotor represented by an Actuator Disk (AD) immersed in domain mesh:

- Based on Froude's AD concept (5), with uniform normal loading;

WT wake modelling in VENTOS[®]/2...

Wind Turbine (WT) rotor represented by an Actuator Disk (AD) immersed in domain mesh:

- Based on Froude's AD concept (5), with uniform normal loading;
- WT(s) drag implicitly calculated during RaNS solver iteration, using 1-D momentum theory and feeding from intermediate case solution (2);

WT wake modelling in VENTOS[®]/2...

Wind Turbine (WT) rotor represented by an Actuator Disk (AD) immersed in domain mesh:

- Based on Froude's AD concept (5), with uniform normal loading;
- WT(s) drag implicitly calculated during RaNS solver iteration, using 1-D momentum theory and feeding from intermediate case solution (2);
- Estimates WT's equivalent free-stream velocity U_{∞} and power output;

WT wake modelling in VENTOS[®]/2...

Wind Turbine (WT) rotor represented by an Actuator Disk (AD) immersed in domain mesh:

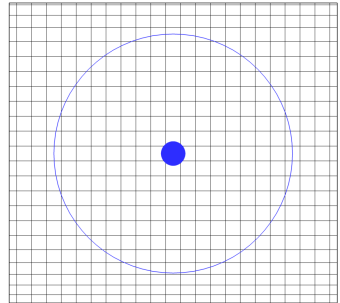
- Based on Froude's AD concept (5), with uniform normal loading;
- WT(s) drag implicitly calculated during RaNS solver iteration, using 1-D momentum theory and feeding from intermediate case solution (2);
- Estimates WT's equivalent free-stream velocity U_∞ and power output;
- Requires only basic WT make/model data: thrust coefficient (C_T) curve, rotor diameter, hub height;

WT wake modelling in VENTOS®/2...

Wind Turbine (WT) rotor represented by an Actuator Disk (AD) immersed in domain mesh:

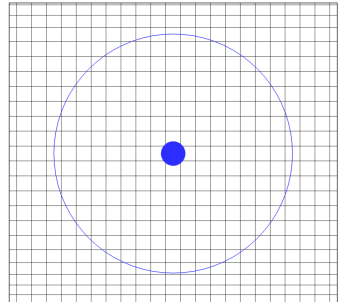
- Based on Froude's AD concept (5), with uniform normal loading;
- WT(s) drag implicitly calculated during RaNS solver iteration, using 1-D momentum theory and feeding from intermediate case solution (2);
- Estimates WT's equivalent free-stream velocity U_∞ and power output;
- Requires only basic WT make/model data: thrust coefficient (C_T) curve, rotor diameter, hub height;
- AD rotates towards inflow;

Smooth discretization of WT drag over course mesh



Smooth discretization of WT drag over course mesh

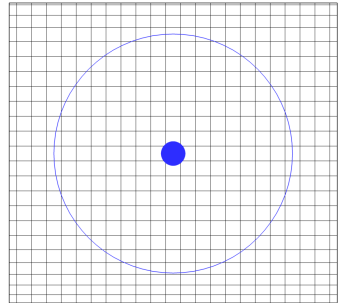
- 1 Approximate disk velocity \mathbf{U}_{disk} as hub position velocity, interpolated from intermediate solution;



Smooth discretization of WT drag over course mesh

- ① Approximate disk velocity \mathbf{U}_{disk} as hub position velocity, interpolated from intermediate solution;
- ② Iterate momentum theory's \mathbf{C}_T definition with manufacturer's curve until convergence on a $\mathbf{U}_{\infty}/\mathbf{C}_T$ pair:

$$\mathbf{C}_T = 4a(1 - a) \quad , \text{with} \quad a = 1 - \frac{\mathbf{U}_{\text{disk}}}{\mathbf{U}_{\infty}}$$



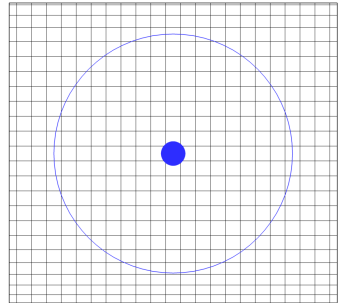
Smooth discretization of WT drag over course mesh

- 1 Approximate disk velocity \mathbf{U}_{disk} as hub position velocity, interpolated from intermediate solution;
- 2 Iterate momentum theory's \mathbf{C}_T definition with manufacturer's curve until convergence on a $\mathbf{U}_\infty/\mathbf{C}_T$ pair:

$$\mathbf{C}_T = 4a(1 - a) \text{ , with } a = 1 - \frac{\mathbf{U}_{\text{disk}}}{\mathbf{U}_\infty}$$

- 3 Determine total thrust:

$$\mathbf{T} = \frac{1}{2} \rho \mathbf{C}_T A_d \mathbf{U}_\infty^2$$



Smooth discretization of WT drag over course mesh

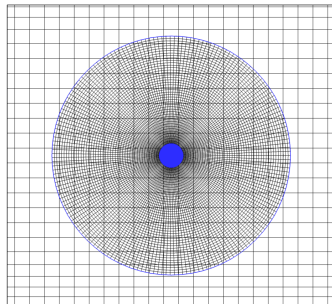
- ① Approximate disk velocity \mathbf{U}_{disk} as hub position velocity, interpolated from intermediate solution;
- ② Iterate momentum theory's \mathbf{C}_T definition with manufacturer's curve until convergence on a $\mathbf{U}_{\infty}/\mathbf{C}_T$ pair:

$$\mathbf{C}_T = 4a(1 - a) \text{ , with } a = 1 - \frac{\mathbf{U}_{\text{disk}}}{\mathbf{U}_{\infty}}$$

- ③ Determine total thrust:

$$\mathbf{T} = \frac{1}{2} \rho \mathbf{C}_T A_d \mathbf{U}_{\infty}^2$$

- ④ Uniformly distribute \mathbf{T} over high-resolution description of virtual rotor in cylindrical coordinates;



Smooth discretization of WT drag over course mesh

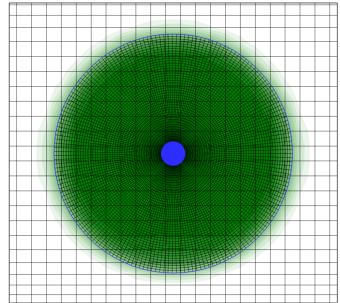
- ① Approximate disk velocity \mathbf{U}_{disk} as hub position velocity, interpolated from intermediate solution;
- ② Iterate momentum theory's \mathbf{C}_T definition with manufacturer's curve until convergence on a $\mathbf{U}_{\infty}/\mathbf{C}_T$ pair:

$$\mathbf{C}_T = 4a(1 - a) \text{ , with } a = 1 - \frac{\mathbf{U}_{\text{disk}}}{\mathbf{U}_{\infty}}$$

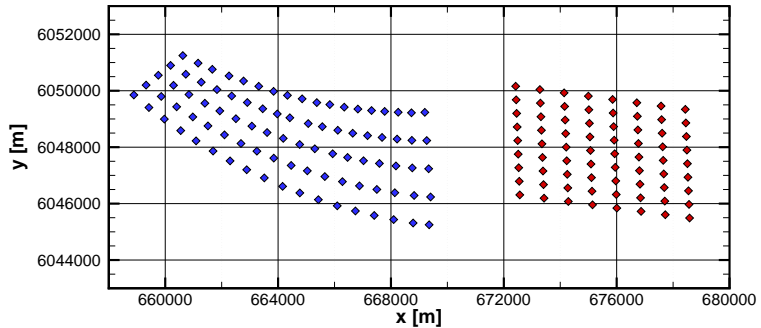
- ③ Determine total thrust:

$$\mathbf{T} = \frac{1}{2} \rho \mathbf{C}_T A_d \mathbf{U}_{\infty}^2$$

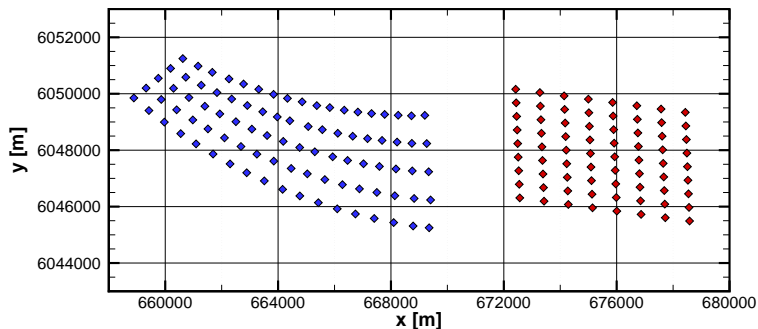
- ④ Uniformly distribute \mathbf{T} over high-resolution description of virtual rotor in cylindrical coordinates;
- ⑤ Extrapolate F_n distribution from virtual rotor sink terms in momentum equations.



Assess wind farm wakes inside a cluster



Assess wind farm wakes inside a cluster



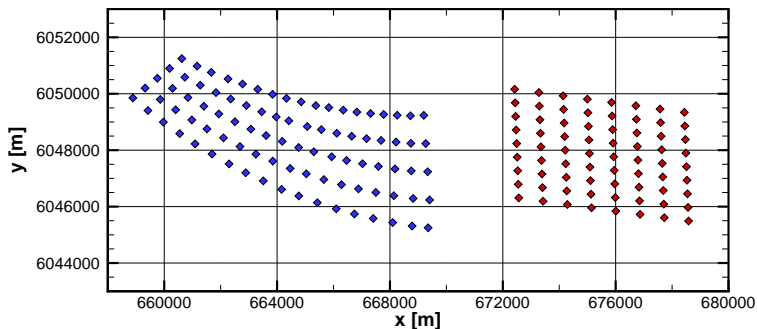
Rødsand 2:

5×18 WT_s

Siemens 2.3MW/92.6m machines

Internal spacing: 5-10D

Assess wind farm wakes inside a cluster



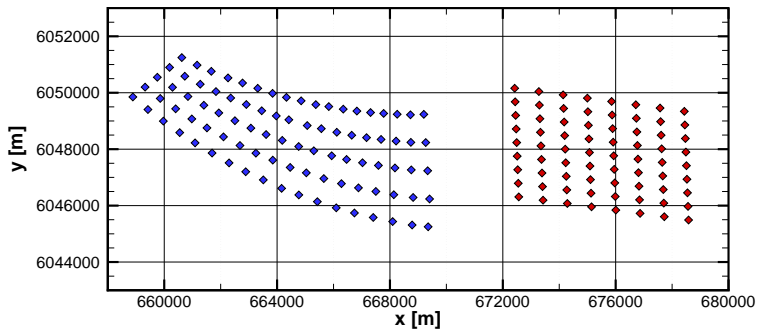
Rødsand 2:

5×18 WTs
Siemens 2.3MW/92.6m machines
Internal spacing: 5-10D

Nysted:

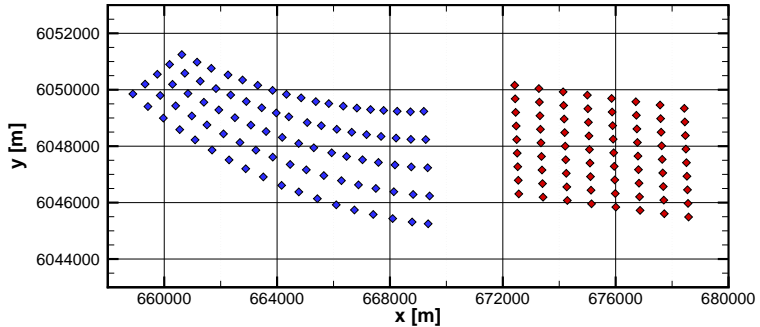
9×8 WTs
Bonus 2.3MW/82.4m machines
Internal spacing: 5.7D, 10.3D

Assess wind farm wakes inside a cluster



Westerly winds: Rødsand 2

Assess wind farm wakes inside a cluster



Westerly winds: Rødsand 2

Easterly winds: Nysted + Rødsand 2

20+ km and 152 WT's to model!

Computational costs

To solve all ADs consistently, wind farm has to be resolved with a minimum of $D/4$ resolution in the horizontal plane.

Computational costs

To solve all ADs consistently, wind farm has to be resolved with a minimum of $D/4$ resolution in the horizontal plane.

On 8-core intel processors:

To solve all ADs consistently, wind farm has to be resolved with a minimum of $D/4$ resolution in the horizontal plane.

- Westerly winds (Rødsand 2): 7-8M cells, solution in 0.5-1 days wallclock time;

Computational costs

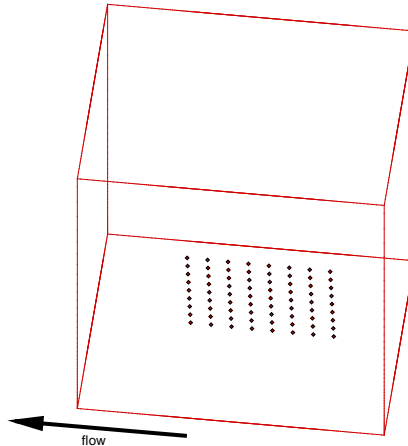
To solve all ADs consistently, wind farm has to be resolved with a minimum of $D/4$ resolution in the horizontal plane.

On 8-core intel processors:

- Westerly winds (Rødsand 2): 7-8M cells, solution in 0.5-1 days wallclock time;
- Easterly winds (Nysted + Rødsand 2): around 20M cells, computational cost very high with strong probability of convergence issues.

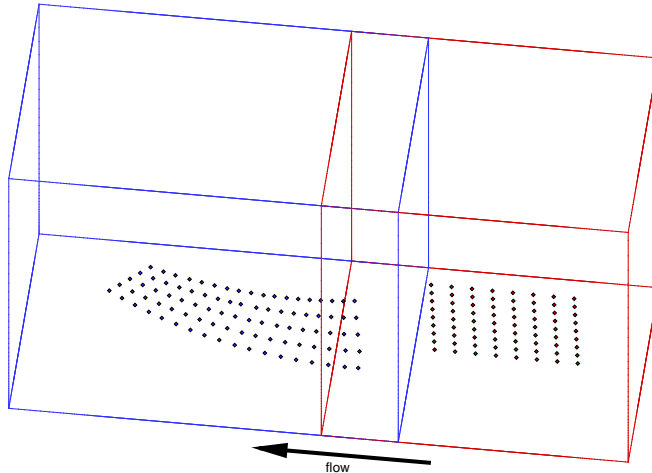
Solution: Break up larger domains into two cases

Precursor solution



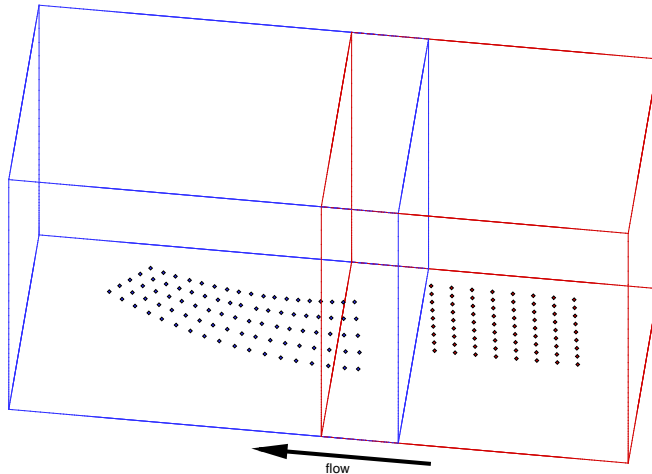
Precursor domain includes upstream wind farm

Precursor solution



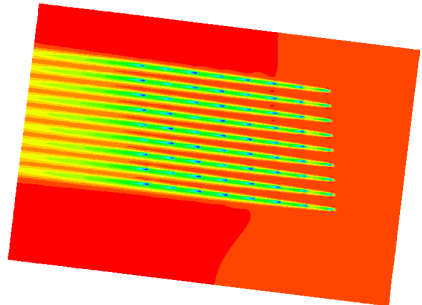
Two domains partially super-impose

Precursor solution



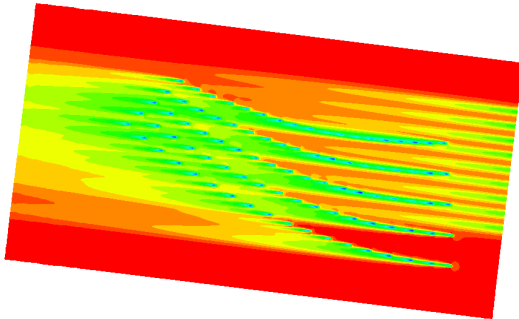
Total computational cost: 6M + 7-8M cells,
0.5 + 1-1.5 days wallclock time;

Precursor solution



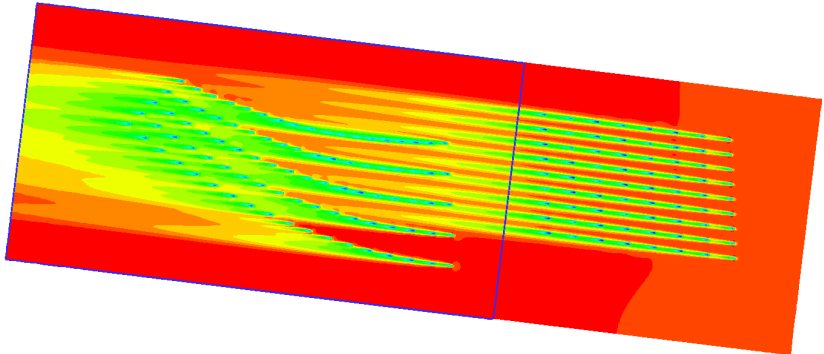
Solution to precursor case

Precursor solution



Use precursor as source for inlet conditions

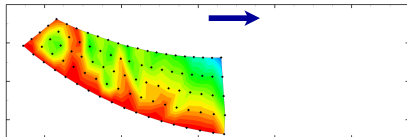
Precursor solution



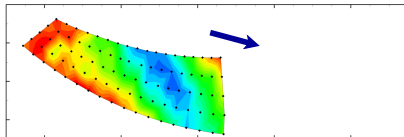
Solution to full case

Model results: Westerly winds, "clean" inflow

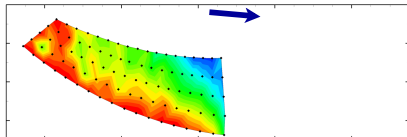
270°:



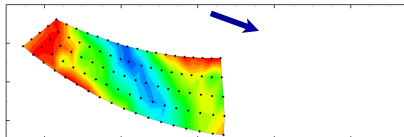
285°:



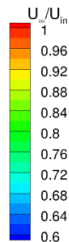
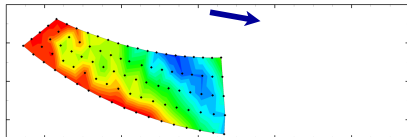
275°:



290°:

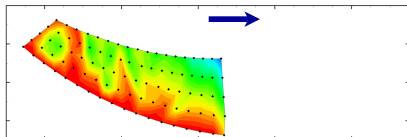


280°:

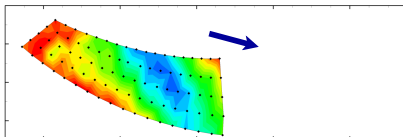


Model results: Westerly winds, "clean" inflow

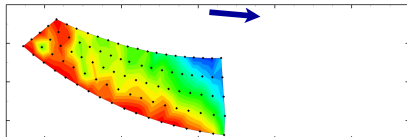
270°:



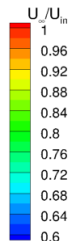
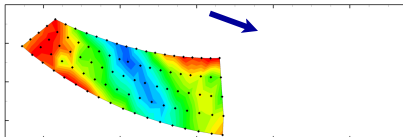
285°:



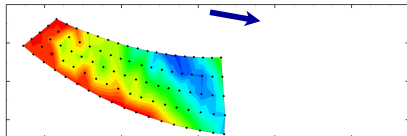
275°:



290°:



280°:

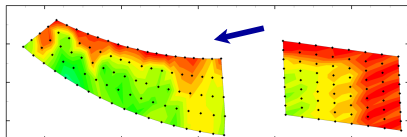


$P_{Avg.}/P_{Ref.WT}$ in Rødsand II

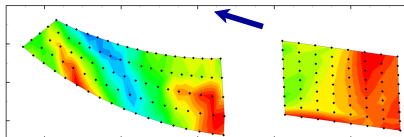
270°	275°	280°	285°	290°
0.80	0.63	0.56	0.56	0.64

Model results: Easterly winds, "waked" inflow

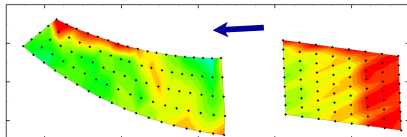
77°:



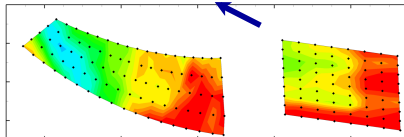
107°:



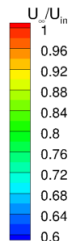
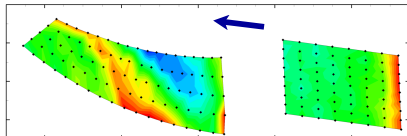
87°:



117°:

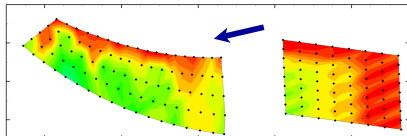


97°:

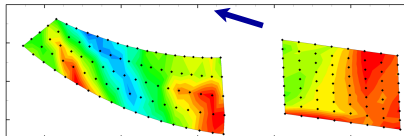


Model results: Easterly winds, "waked" inflow

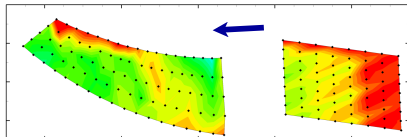
77°:



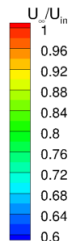
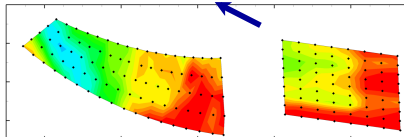
107°:



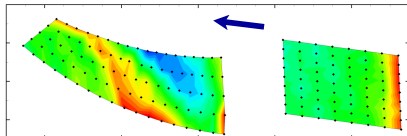
87°:



117°:



97°:



$P_{Avg.}/P_{Ref.WT}$ in Rødsand II

77°	87°	97°	107°	117°
0.65	0.54	0.52	0.55	0.65

Concluding

- RaNS-base wake model capable of modelling a large number of WT in a single simulation;

Concluding

- RaNS-base wake model capable of modelling a large number of WT in a single simulation;
- Wake modelling at the WF cluster scale is possible, with careful selection of precursor simulations to produce inflow data;

Concluding

- RaNS-base wake model capable of modelling a large number of WT in a single simulation;
- Wake modelling at the WF cluster scale is possible, with careful selection of precursor simulations to produce inflow data;
- Wake modelling at the WF cluster scale is possible with reasonable computational effort and little loss of code stability;

Concluding

- RaNS-base wake model capable of modelling a large number of WT in a single simulation;
- Wake modelling at the WF cluster scale is possible, with careful selection of precursor simulations to produce inflow data;
- Wake modelling at the WF cluster scale is possible with reasonable computational effort and little loss of code stability;
- Single WT U_∞ over-estimation leads to deficit over-estimation, with cumulative effects in a WF;

Concluding

- RaNS-base wake model capable of modelling a large number of WT in a single simulation;
- Wake modelling at the WF cluster scale is possible, with careful selection of precursor simulations to produce inflow data;
- Wake modelling at the WF cluster scale is possible with reasonable computational effort and little loss of code stability;
- Single WT U_{∞} over-estimation leads to deficit over-estimation, with cumulative effects in a WF;
- Curved WT rows in Rødsand II means WF efficiency is strongly dependent on inflow direction;

Concluding

- RaNS-base wake model capable of modelling a large number of WT in a single simulation;
- Wake modelling at the WF cluster scale is possible, with careful selection of precursor simulations to produce inflow data;
- Wake modelling at the WF cluster scale is possible with reasonable computational effort and little loss of code stability;
- Single WT U_{∞} over-estimation leads to deficit over-estimation, with cumulative effects in a WF;
- Curved WT rows in Rødsand II means WF efficiency is strongly dependent on inflow direction;
- Easterly sector winds show a strong effect of Nysted WF on Rødsand II's entry WTs, effect extending to the inner WTs.

References

- [1] F. Castro, J. Palma, and A. Silva Lopes. Simulation of the askervein flow. part 1: Reynolds averaged navier–stokes equations ($k \in$ turbulence model). *Boundary-Layer Meteorology*, 107(3):501–530, 2003.
- [2] V. M. M. G. C. Gomes, J. M. L. M. Palma, and A. S. Lopes. Improving actuator disk wake model. *Journal of Physics: Conference Series*, 524(1):012170, 2014.
- [3] P. H. Madsen and C. Hasager. Eera design tool for offshore wind farm cluster (dtoc), March 2015. Presented at EWEA Offshore 2015 event, 10 March 2015, Copenhagen.
- [4] J. Palma, F. Castro, L. Ribeiro, A. Rodrigues, and A. Pinto. Linear and nonlinear models in wind resource assessment and wind turbine micro-siting in complex terrain. *Journal of Wind Engineering and Industrial Aerodynamics*, 96(12):2308 – 2326, 2008.
- [5] G. Van Kuik. *On the Limitations of Froude’s Actuator Disc Concept*. PhD thesis, Technical University of Eindhoven, 1991.